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TPS61071-Q1

SLVSAA5A –MAY 2010–REVISED DECEMBER 2015

TPS61071-Q1 90% Efficient Synchronous Boost Converter With 600-mA Switch

1 Features

- Qualified for Automotive Applications
- AEC-Q100 Qualified With the Following Results:
  - Device Temperature Grade 2: –40°C to 105°C Ambient Operating Temperature Range
  - Device HBM Classification Level 1C
  - Device CDM Classification Level C6
- 90% Efficient Synchronous Boost Converter
  - 75-mA Output Current at 3.3 V From 0.9-V Input
  - 150-mA Output Current at 3.3 V From 1.8-V Input
- Device Quiescent Current: 19 µA (Typical)
- Input Voltage Range: 0.9 V to 5.5 V
- Adjustable Output Voltage Up to 5.5 V
- Power-Save Mode Version Available for Improved Efficiency at Low Output Power
- Load Disconnect During Shutdown
- Overtemperature Protection
- Small 6-Pin Thin SOT Package

2 Applications

- Automotive Power Supplies
- Boost Power Supplies

3 Description

The TPS61071-Q1 device provides a power supply solution for products powered by lower-voltage DC rails or a one-cell, two-cell, or three-cell alkaline, NiCd or NiMH, or one-cell Li-ion or Li-polymer battery. Output currents can go as high as 75 mA, while using a single-cell alkaline, and discharge down to 0.9 V. The device can also generate 5 V at 200 mA from a 3.3-V rail or a Li-ion battery. The boost converter is based on a fixed frequency, pulse-width-modulation (PWM) controller using a synchronous rectifier to obtain maximum efficiency. The maximum peak current in the boost switch is limited typically to a value of 600 mA.

The TPS61071-Q1 output voltage is programmed by an external resistor divider. To minimize battery drain, disable the converter. During shutdown, the load disconnects from the battery. The device package is a 6-pin thin SOT package (DDC).

Device Information[1]

PART NUMBER	PACKAGE	BODY SIZE (NOM)
TPS61071-Q1	SOT (6)	1.60 mm × 2.90 mm

(1) For all available packages, see the orderable addendum at the end of the data sheet.
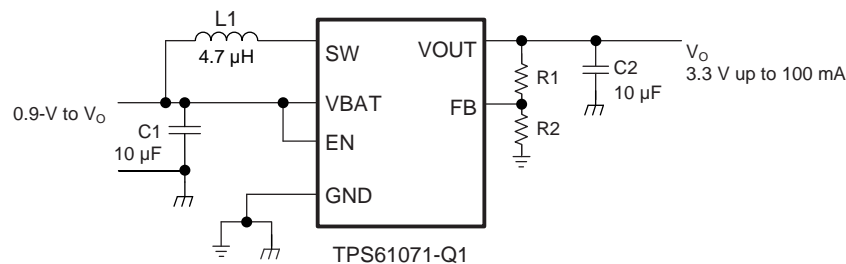
Typical Application Circuit
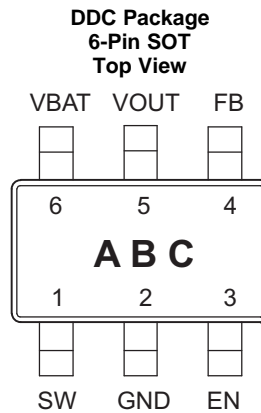
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4 Revision History

NOTE: Page numbers for previous revisions may differ from page numbers in the current version.

Changes from Original (May 2010) to Revision A   **Page**

5 Pin Configuration and Functions

DDC Package
6-Pin SOT
Top View

Pin Functions

PIN		I/O	DESCRIPTION
NO.	NAME		
1	SW	I	Boost and rectifying switch input
2	GND	—	Device (IC) ground connection for logic and power
3	EN	I	Enable input (1/VBAT enabled, 0/GND disabled)
4	FB	I	Voltage feedback for programming the output voltage
5	VOUT	O	Boost converter output
6	VBAT	I	Supply voltage

6 Specifications

6.1 Absolute Maximum Ratings

over operating free-air temperature range (unless otherwise noted)[1]

	MIN	MAX	UNIT
Input voltage range on SW, VOUT, VBAT, EN, FB	−0.3	7	V
Operating virtual junction temperature, T_J	−40	150	°C
Storage temperature, T_{stg}	−65	150	°C

(1) Stresses beyond those listed under *Absolute Maximum Ratings* may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated under *Recommended Operating Conditions* is not implied. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

6.2 ESD Ratings

			VALUE	UNIT
$V_{(ESD)}$	Electrostatic discharge	Human-body model (HBM), per AEC Q100-002[1]	±2000	V
		Charged-device model (CDM), per AEC Q100-011	±1000	

(1) AEC Q100-002 indicates that HBM stressing shall be in accordance with the ANSI/ESDA/JEDEC JS-001 specification.

6.3 Recommended Operating Conditions

	MIN	NOM	MAX	UNIT
Supply voltage at VBAT, V_I	0.9		5.5	V
Operating free air temperature range, T_A	−40		105	°C
Operating virtual junction temperature range, T_J	−40		125	°C

6.4 Thermal Information

THERMAL METRIC[1]		TPS61071-Q1	UNIT
		DDC (SOT)	
		6 PINS	
$R_{\theta JA}$	Junction-to-ambient thermal resistance	139.1	°C/W
$R_{\theta JC(top)}$	Junction-to-case (top) thermal resistance	34.8	°C/W
$R_{\theta JB}$	Junction-to-board thermal resistance	42.5	°C/W
ψ_{JT}	Junction-to-top characterization parameter	1.4	°C/W
ψ_{JB}	Junction-to-board characterization parameter	40.7	°C/W
$R_{\theta JC(bot)}$	Junction-to-case (bottom) thermal resistance	N/A	°C/W

(1) For more information about traditional and new thermal metrics, see the *Semiconductor and IC Package Thermal Metrics* application report, SPRA953.

6.5 Electrical Characteristics

over recommended free-air temperature range and over recommended input voltage range (typical at an ambient temperature range of 25°C) (unless otherwise noted)

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
DC-DC STAGE						
V_I	Minimum input voltage range for start-up	R_L = 270 Ω		1.1	1.25	V
	Input voltage range, after start-up	T_A = 25°C	0.9		5.5	
V_O	Output voltage range			1.8	5.5	V
$V_{(FB)}$	Feedback voltage	T_A = 25°C	490	500	510	mV
f	Oscillator frequency		960	1200	1440	kHz
$I_{(SW)}$	Switch current limit	VOUT= 3.3 V	455	600	735	mA
	Start-up current limit			0.5 × I_{SW}		mA
	Boost switch-on resistance	VOUT= 3.3 V		480		mΩ
	Rectifying switch-on resistance	VOUT= 3.3 V		600		mΩ
	Total accuracy (including line and load regulation)				5%	
	Line regulation			1%		
	Load regulation			1%		
Quiescent current	VBAT	I_O= 0 mA, $V_{(EN)}$= VBAT = 1.2 V, VOUT = 3.3 V, T_A = 25°C		0.5	1	μA
	VOUT			190[1]	300[1]	
				20[2]		
	Shutdown current	$V_{(EN)}$ = 0 V, VBAT = 1.2 V, T_A = 25°C		0.05	0.5	μA
CONTROL STAGE						
$V_{(UVLO)}$	Undervoltage lockout threshold	$V_{(BAT)}$ voltage decreasing		0.8		V
V_{IL}	EN input low voltage				0.2 × VBAT	V
V_{IH}	EN input high voltage		0.8 × VBAT			V
	EN input current	Clamped on GND or VBAT		0.01	0.1	μA
	Overtemperature protection			140		°C
	Overtemperature hysteresis			20		°C

(1) Switching current
(2) Non-switching current

6.6 Typical Characteristics

Table 1. Table of Graphs

		FIGURE
Maximum output current	vs Input voltage	Figure 1
Efficiency	vs Output current	Figure 2
	vs Output current	Figure 3
	vs Output current	Figure 4
	vs Input voltage	Figure 5
	vs Input voltage	Figure 6
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Waveforms	Output voltage in continuous mode	Figure 10
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	Load transient response	Figure 12
	Load transient response	Figure 13
	Line transient response	Figure 14
	Line transient response	Figure 15
	Start-up after enable	Figure 16
	Start-up after enable	Figure 17
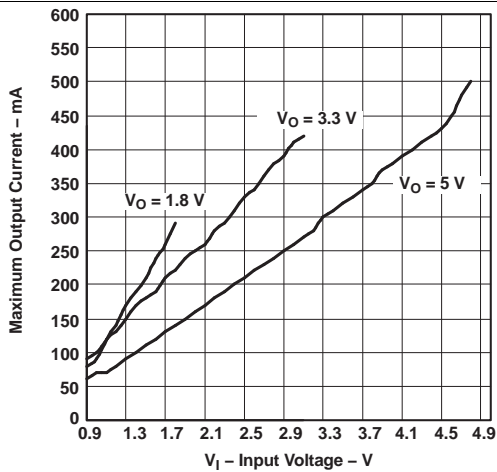
Figure 1. Maximum Output Current vs Input Voltage

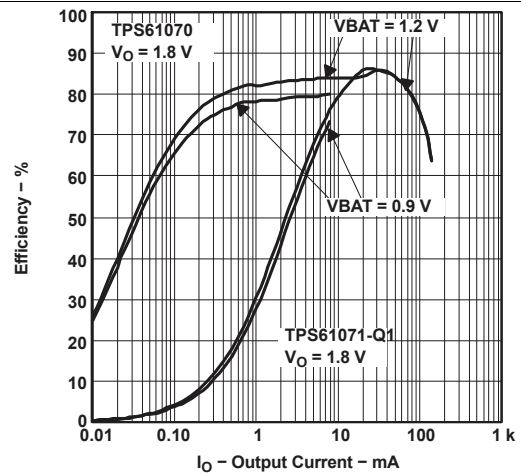**Figure 2. Efficiency vs Output Current**
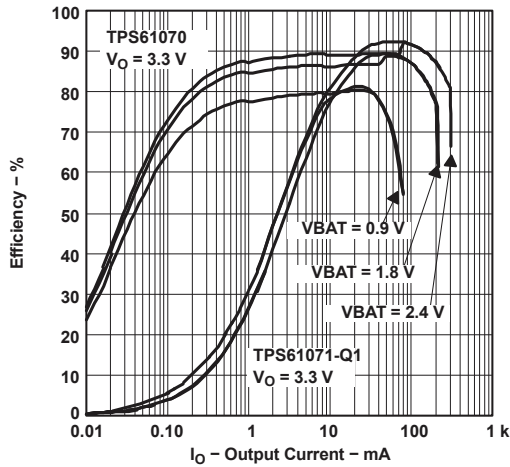
Product Folder Links: *TPS61071-Q1*
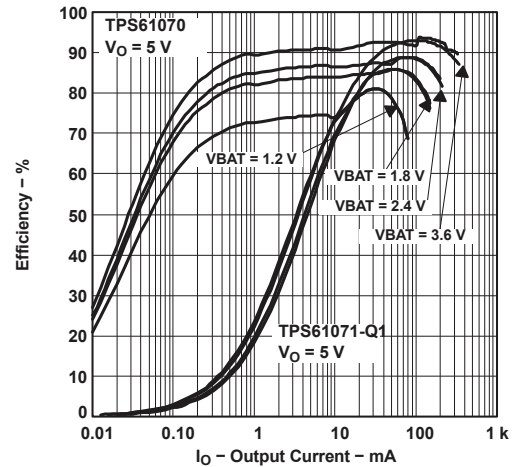
Figure 3. Efficiency vs Output Current

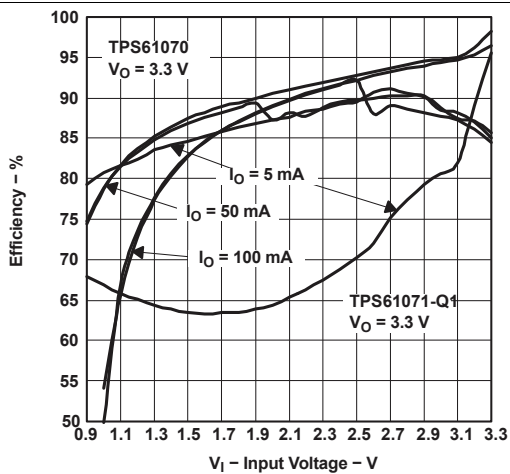Figure 4. Efficiency vs Output Current
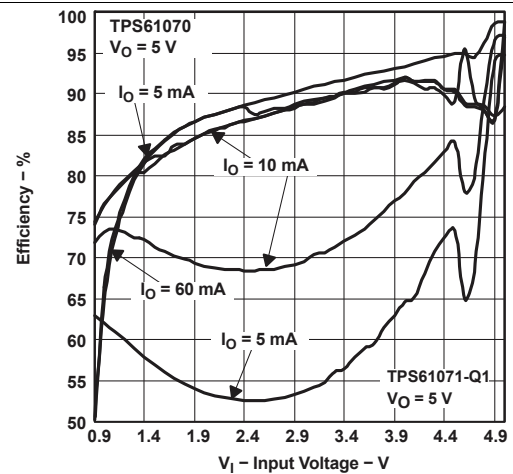

Figure 5. Efficiency vs Input Voltage

Figure 6. Efficiency vs Input Voltage
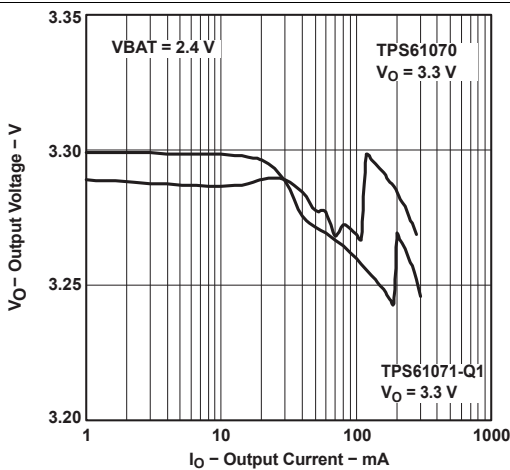
Figure 7. Output Voltage vs Output Current
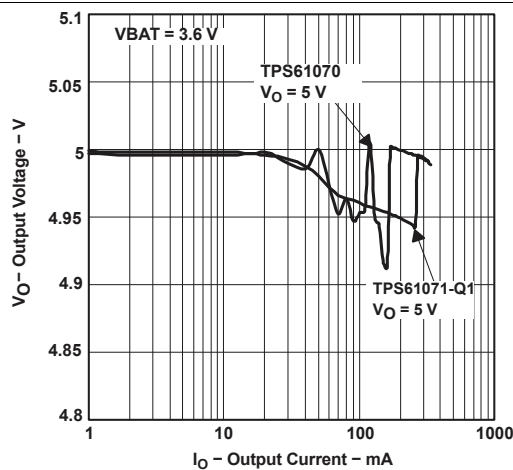
Figure 8. Output Voltage vs Output Current

Product Folder Links: TPS61071-Q1
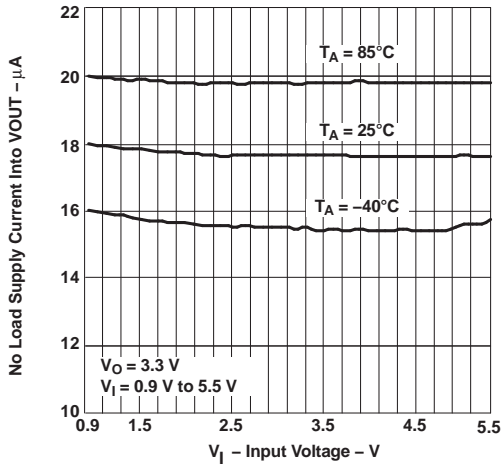
Figure 9. No Load Supply Current Into V_{OUT} vs Input Voltage

Figure 10. TPS61071 Output Voltage in Continuous Mode

Figure 11. TPS61071 Output Voltage in Continuous Mode

Figure 12. TPS61071 Load Transient Response
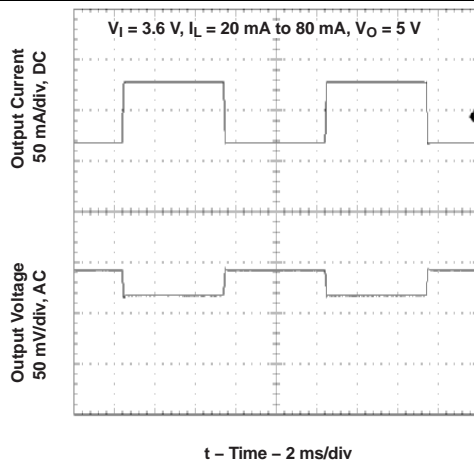
Figure 13. TPS61071 Load Transient Response
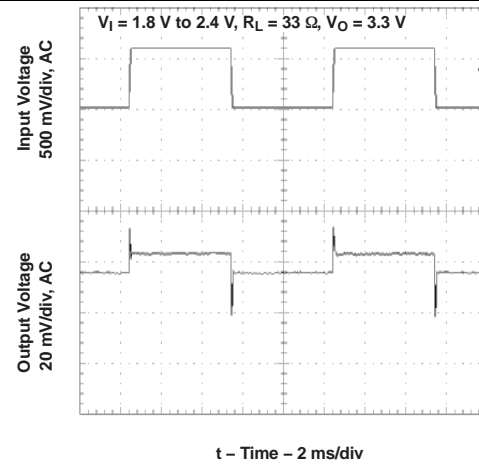
Figure 14. TPS61071 Line Transient Response

Product Folder Links: *TPS61071-Q1*
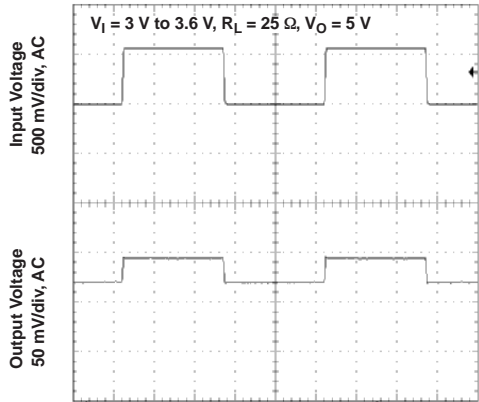
Figure 15. TPS61071 Line Transient Response
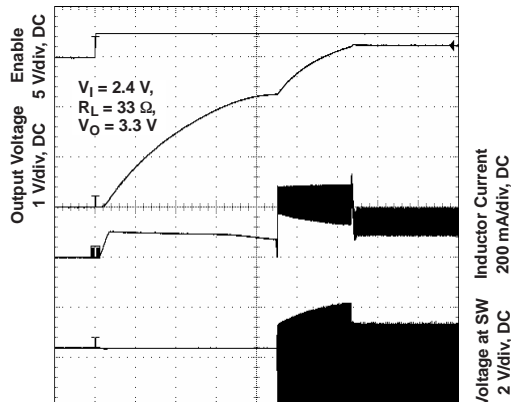
Figure 16. TPS61071 Start-Up After Enable
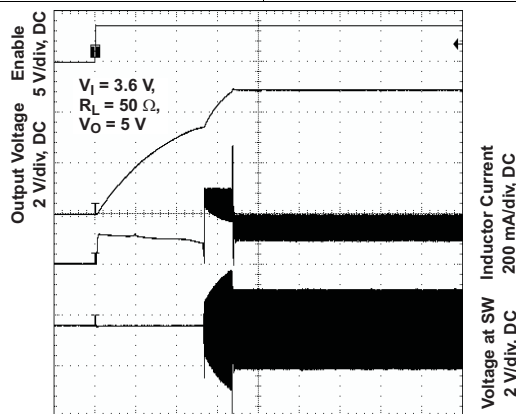
Figure 17. TPS61071 Start-Up After Enable

7 Detailed Description

7.1 Overview

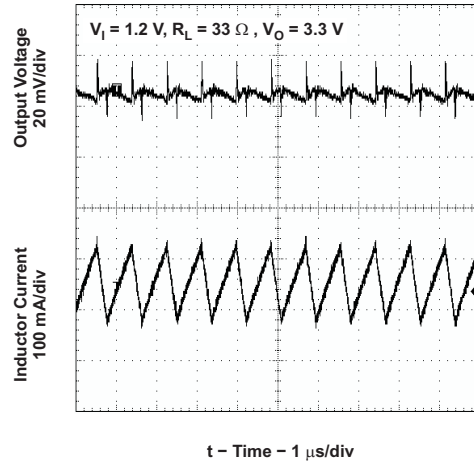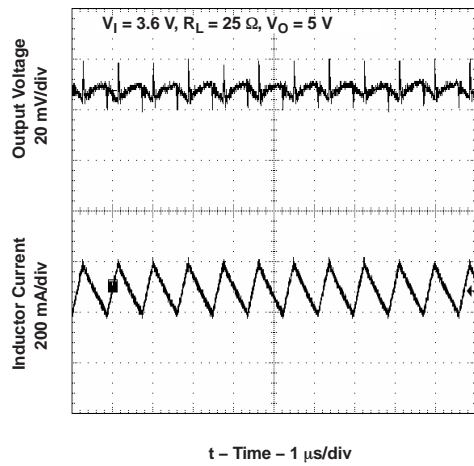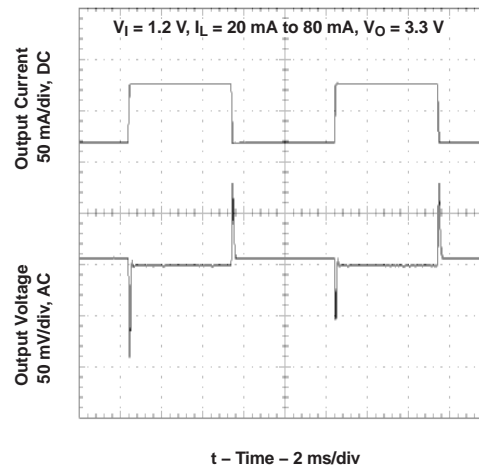The TPS61071-Q1 provides a boost power supply solution for products powered by either DC supply rails or batteries such as one-cell, two-cell, or three-cell alkaline, NiCd or NiMH, or one-cell Li-ion or Li-polymer battery. Output currents can go as high as 75 mA, while using a single-cell alkaline, and discharge down to 0.9 V. The device can also generate 5 V at 200 mA from a 3.3-V rail or a Li-ion battery. The boost converter is based on a fixed frequency, pulse-width modulation (PWM) controller using a synchronous rectifier to obtain maximum efficiency. The TPS61071-Q1 does not have a POWER-SAVE mode. Even with low-load currents, the device is forced to operate at the fixed switching frequency. The maximum peak current in the boost switch is limited typically to a value of 600 mA. An external-resistor divider programs the output voltage. To minimize battery drain, disable the converter. During shutdown, the load disconnects from the battery.

7.2 Functional Block Diagram
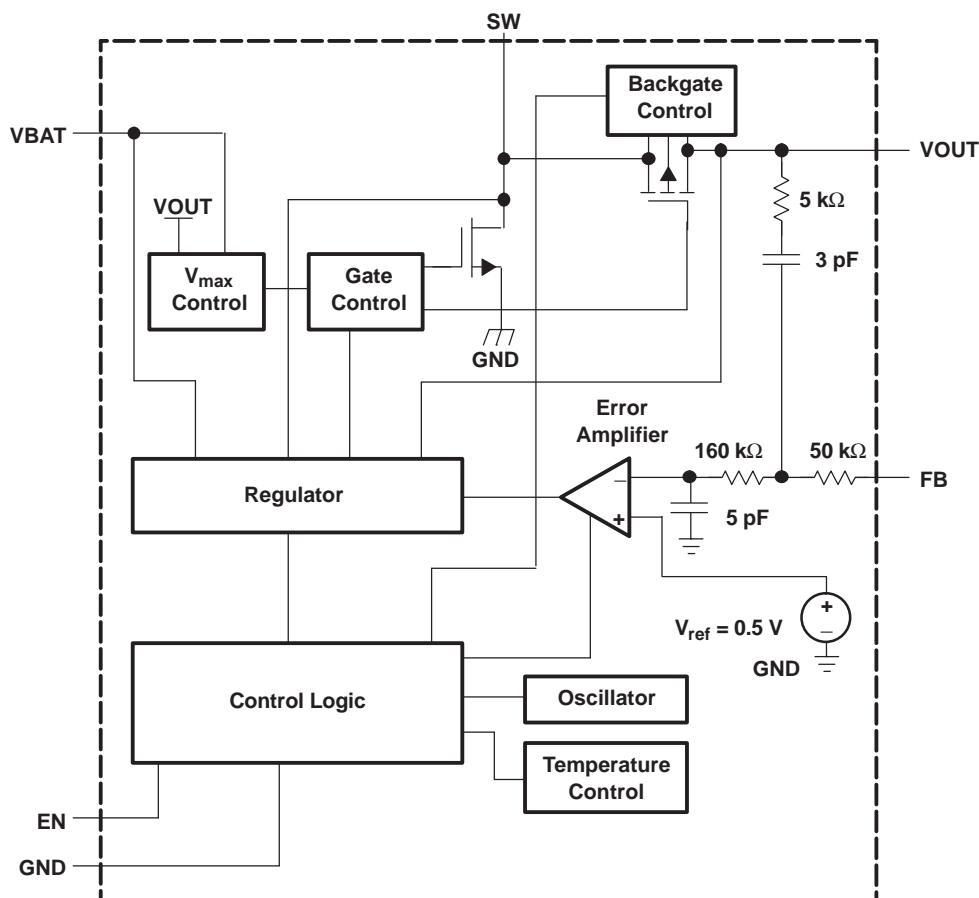
7.3 Feature Description

7.3.1 Controller Circuit

The controller circuit of the device is based on a fixed-frequency multiple feed-forward controller topology. Input voltage, output voltage, and voltage drop on the NMOS switch are monitored and forwarded to the regulator. So, changes in the operating conditions of the converter directly affect the duty cycle and must not take the indirect and slow way through the control loop and the error amplifier. The control loop, determined by the error amplifier, only has to handle small signal errors. The input for it is the feedback voltage on the FB pin. It is compared with the internal reference voltage to generate an accurate and stable output voltage.

The peak current of the NMOS switch is also sensed to limit the maximum current flowing through the switch and the inductor. The typical peak-current limit is set to 600 mA. An internal temperature sensor prevents the device from getting overheated in case of excessive power dissipation.

7.3.1.1 Synchronous Rectifier

The device integrates an N-channel and a P-channel MOSFET transistor to realize a synchronous rectifier. Because the commonly used discrete Schottky rectifier is replaced with a low $R_{DS(on)}$ PMOS switch, the power conversion efficiency reaches values above 90%. A special circuit is applied to disconnect the load from the input during shutdown of the converter. In conventional synchronous rectifier circuits, the backgate diode of the high-side PMOS is forward biased in shutdown and allows current flowing from the battery to the output. However, this device uses a special circuit, which takes the cathode of the backgate diode of the high-side PMOS and disconnects it from the source when the regulator is not enabled (EN = low).

The benefit of this feature for the system design engineer is that the battery is not depleted during shutdown of the converter. No additional components must be added to the design to make sure that the battery is disconnected from the output of the converter.

7.3.1.2 Undervoltage Lockout

An undervoltage lockout function prevents the device from operating if the supply voltage on VBAT is lower than approximately 0.8 V. When in operation and the battery is being discharged, the device automatically enters the shutdown mode if the voltage on VBAT drops below approximately 0.8 V. This undervoltage lockout function is implemented in order to prevent the malfunctioning of the converter.

7.3.1.3 Soft Start and Short-Circuit Protection

When the device enables, the internal start-up cycle starts with the first step, the precharge phase. During precharge, the rectifying switch is turned on until the output capacitor is charged to a value close to the input voltage. The rectifying switch is current limited during this phase. The current limit increases with the output voltage. This circuit also limits the output current under short-circuit conditions at the output. Figure 18 shows the typical precharge current vs output voltage for specific input voltages:
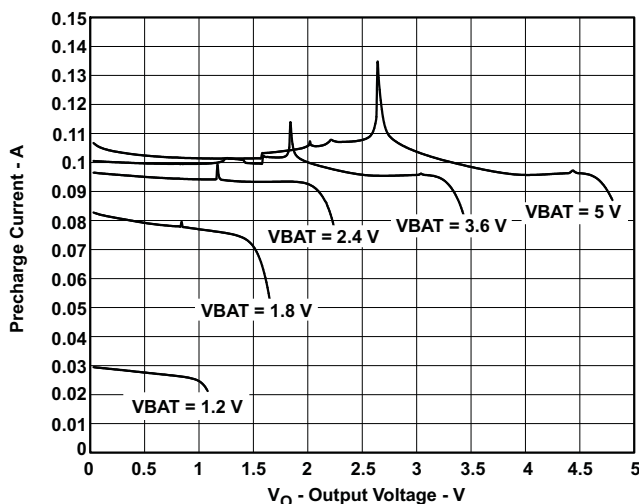
Figure 18. Precharge and Short Circuit Current

Feature Description (continued)

After charging the output capacitor to the input voltage, the device starts switching. If the input voltage is below 1.8 V, the device works with a fixed duty cycle of 70% until the output voltage reaches 1.8 V. After that the duty cycle is set depending on the input output voltage ratio. Until the output voltage reaches its nominal value, the boost switch current limit is set to 50% of its nominal value to avoid high peak currents at the battery during start-up. As soon as the output voltage is reached, the regulator takes control, and the switch current limit is set back to 100%.

7.4 Device Functional Modes

7.4.1 Device Enable

The device is put into operation when EN is set high and put into a SHUTDOWN mode when EN is set to GND. In SHUTDOWN mode, the regulator stops switching, all internal control circuitry switches off, and the device isolates the load from the input (see *Synchronous Rectifier*). This also means that the output voltage can drop below the input voltage during shutdown. During start-up of the converter, the duty cycle and the peak current are limited to avoid high-peak currents drawn from the battery.

8 Application and Implementation

> **NOTE**
>
> Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes. Customers should validate and test their design implementation to confirm system functionality.

8.1 Application Information

The TPS61071-Q1 DC-DC converter is intended for systems powered by a single-cell, up to triple-cell alkaline, NiCd, NiMH battery with a typical terminal voltage between 0.9 V and 5.5 V. The TPS61071-Q1 device can also be used in systems powered by one-cell Li-ion or Li-polymer with a typical voltage between 2.5 V and 4.2 V. Additionally, any other voltage source with a typical output voltage between 0.9 V and 5.5 V can power systems where the TPS61071-Q1 is used. Due to the nature of boost converters, the output voltage regulation is only maintained when the input voltage applied is lower than the programmed output voltage.
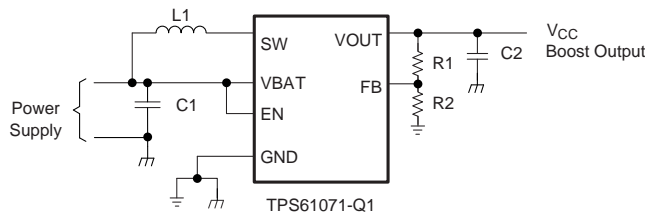
8.2 Typical Applications

Figure 19. Typical Application Circuit

8.2.1 Design Requirements

In this example, TPS61071-Q1 is used to design a 3.3-V power supply with 75-mA output current capability supplied with an input voltage range from 0.9 V to 1.65 V.

8.2.2 Detailed Design Procedure

8.2.2.1 Programming the Output Voltage

The output voltage can be adjusted with an external resistor divider. The typical value of the voltage at the FB pin is 500 mV. The maximum recommended value for the output voltage is 5.5 V. The current through the resistive divider should be about 100 times greater than the current into the FB pin. The typical current into the FB pin is 0.01 µA, and the voltage across R2 is typically 500 mV. Based on those two values, the recommended value for R2 should be lower than 500 kΩ, in order to set the divider current at 1 µA or higher. Because of internal compensation circuitry, the value for this resistor should be in the range of 200 kΩ. From that, the value of resistor R1, depending on the needed output voltage (V_O), is calculated using Equation 1:

$$R1 = R2 \times \left(\frac{V_O}{V_{FB}} - 1 \right) = 180k\Omega \times \left(\frac{V_O}{500mV} - 1 \right) \tag{1}$$

For example, if an output voltage of 3.3 V is needed, a 1 MΩ resistor should be chosen for R1. If for any reason the value chosen for R2 is significantly lower than 200 kΩ, additional capacitance in parallel to R1 is recommended, if the device shows unstable regulation of the output voltage. The required capacitance value is calculated using Equation 2:

$$C_{parR1} = 3 \text{ pF} \times \left(\frac{200 \text{ k}\Omega}{R2} - 1 \right) \tag{2}$$

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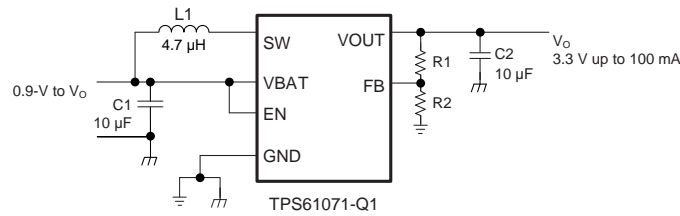
Typical Applications (continued)

Figure 20. Typical Application Circuit for Adjustable Output Voltage Option

8.2.2.2 Inductor Selection L1

A boost converter normally requires two main passive components for storing energy during the conversion. A boost inductor and a storage capacitor at the output are required. To select the boost inductor, it is recommended to keep the possible peak inductor current below the current limit threshold of the power switch in the chosen configuration. For example, the current limit threshold of the TPS61071-Q1's switch is 600 mA. The highest peak current through the inductor and the switch depends on the output load, the input (V_{BAT}), and the output voltage (V_{OUT}). Estimation of the maximum average inductor current is done using Equation 3:

$$L_1 = I_O \times \left(\frac{VOUT}{VBAT \times 0.8} \right)$$

(3)

For example, for an output current of 75 mA at 3.3 V, at least 340 mA of average current flows through the inductor at a minimum input voltage of 0.9 V.

The second parameter for choosing the inductor is the desired current ripple in the inductor. Normally, it is advisable to work with a ripple of less than 20% of the average inductor current. A smaller ripple reduces the magnetic hysteresis losses in the inductor, as well as output voltage ripple and EMI. But in the same way, regulation time rises at load changes. In addition, a larger inductor increases the total system costs. With these parameters, it is possible to calculate the value for the inductor by using Equation 4:

$$L_1 = \frac{VBAT \times (VOUT - VBAT)}{\Delta I_L \times f \times VOUT}$$

(4)

Parameter *f* is the switching frequency and ΔI_L is the ripple current in the inductor, i.e., 40% ΔI_L. In this example, the desired inductor has the value of 4 μH. With this calculated value and the calculated currents, it is possible to choose a suitable inductor. In typical applications, a 4.7-μH inductance is recommended. The device has been optimized to operate with inductance values between 2.2 μH and 10 μH. Nevertheless, operation with higher inductance values may be possible in some applications. Detailed stability analysis is then recommended. Care must be taken because load transients and losses in the circuit can lead to higher currents as estimated in Equation 4. Also, the losses in the inductor caused by magnetic hysteresis losses and copper losses are a major parameter for total circuit efficiency.

Table 2 lists the inductor series from different suppliers which have been used with TPS6107x converters:

Table 2. List of Inductors

VENDOR	INDUCTOR SERIES
TDK	VLF3010
	VLF4012
Wurth Elektronik	744031xxx
	744042xxx
EPCOS	B82462-G4
Cooper Electronics Technologies	SD18
	SD20
Taiyo Yuden	CB2016B xxx
	CB2518B xxx

Product Folder Links: *TPS61071-Q1*

8.2.2.3 *Capacitor Selection*

8.2.2.3.1 Input Capacitor C1

TI recommends at least a 10-µF capacitor to improve transient behavior of the regulator and EMI behavior of the total power supply circuit. A ceramic capacitor or a tantalum capacitor with a 100-nF ceramic capacitor in parallel, placed close to the device, is recommended.

8.2.2.3.2 Output Capacitor C2

The major parameter necessary to define the output capacitor is the maximum allowed output voltage ripple of the converter. This ripple is determined by two parameters of the capacitor, the capacitance and the ESR. To calculate the minimum capacitance needed for the defined ripple, suppose that the ESR is zero and use Equation 5:

$$C_{2(min)} = \frac{I_O \times (VOUT - VBAT)}{f \times \Delta V \times VOUT}$$

where

- Parameter *f* is the switching frequency and ΔV is the maximum allowed ripple.   (5)

With a chosen ripple voltage of 10 mV, a minimum capacitance of 4.5 µF is needed. In this value range, ceramic capacitors are a good choice. The ESR and the additional ripple created are negligible. It is calculated using Equation 6:

$$\Delta V_{ESR} = I_O \times R_{ESR}$$ (6)

The total ripple is the sum of the ripple caused by the capacitance and the ripple caused by the ESR of the capacitor. Additional ripple is caused by load transients. This means that the output capacitor has to completely supply the load during the charging phase of the inductor. The value of the output capacitance depends on the speed of the load transients and the load current during the load change. With the calculated minimum value of 4.5 µF and load transient considerations, the recommended output capacitance value is in a 10 µF range.

Care must be taken on capacitance loss caused by derating due to the applied dc voltage and the frequency characteristic of the capacitor. For example, larger form factor capacitors (in 1206 size) have their self resonant frequencies in the same frequency range as the TPS61071-Q1 operating frequency. So the effective capacitance of the capacitors used may be significantly lower. Therefore, the recommendation is to use smaller capacitors in parallel instead of one larger capacitor.

8.2.2.4 *Small Signal Stability*

To analyze small signal stability in more detail, the small signal transfer function of the error amplifier and the regulator, which is given in Equation 7, can be used:

$$A_{(REG)} = \frac{d}{V_{(FB)}} = \frac{5 \times (R1 + R2)}{R2 \times (1 + i \times \omega \times 0.8\mu s)}$$ (7)

8.2.3 Application Curves

	FIGURE
Output voltage in continuous mode	Figure 21
Output voltage in continuous mode	Figure 22
Load transient response	Figure 23
Load transient response	Figure 24
Line transient response	Figure 25
Line transient response	Figure 26
Start-up after enable	Figure 27
Start-up after enable	Figure 28

Figure 21. TPS61071 Output Voltage in Continuous Mode

Figure 22. TPS61071 Output Voltage In Continuous Mode

Figure 23. TPS61071 Load Transient Response

Figure 24. TPS61071 Load Transient Response

Product Folder Links: *TPS61071-Q1*
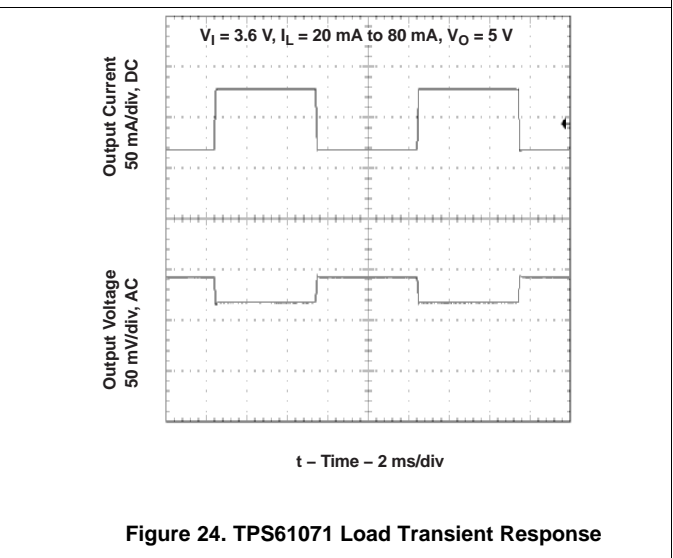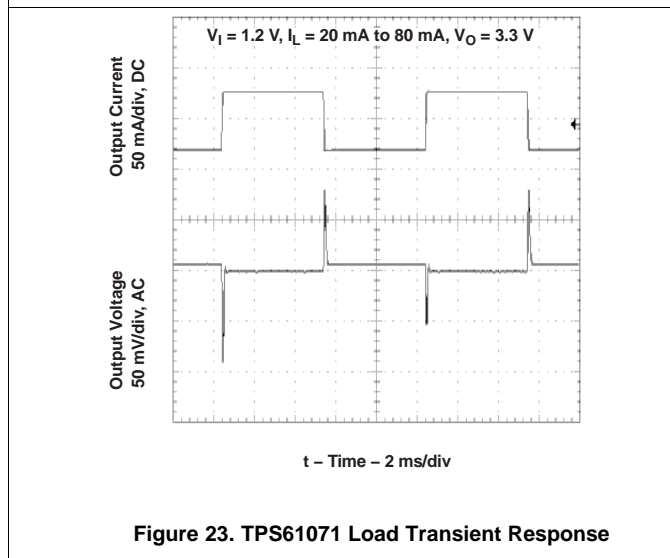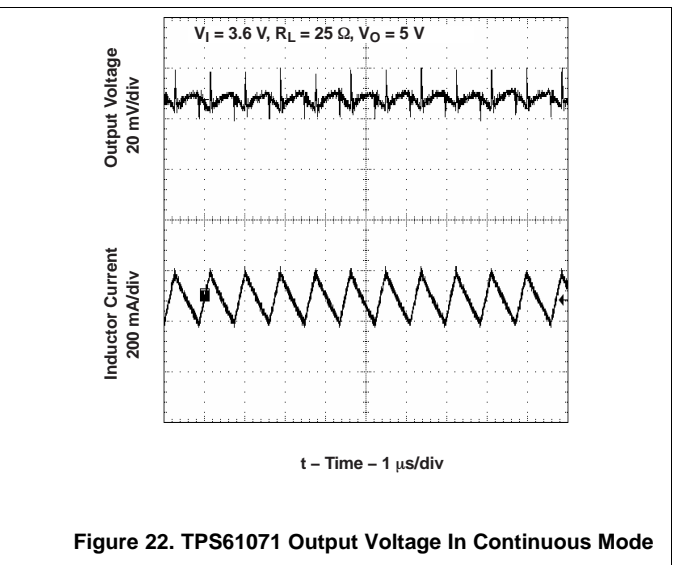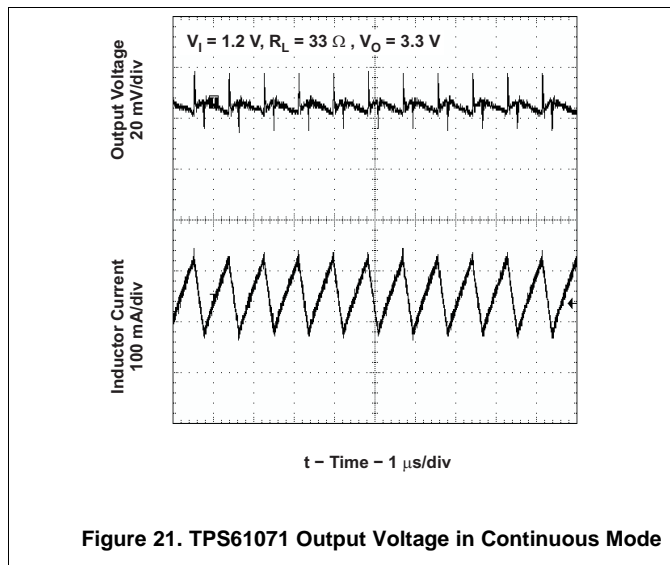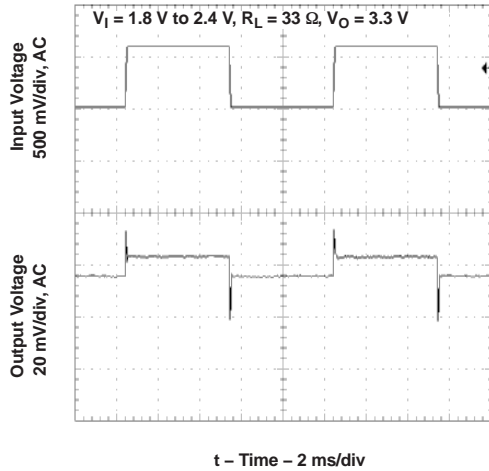
Figure 25. TPS61071 Line Transient Response
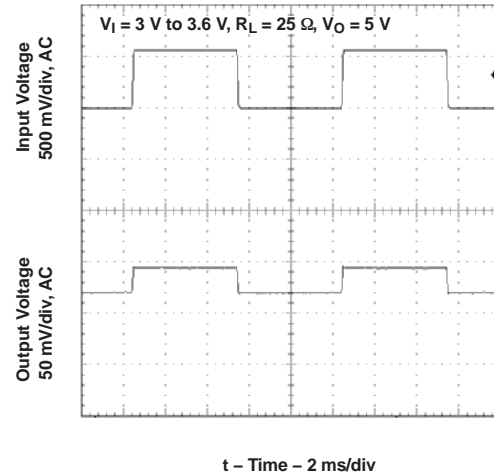
Figure 26. TPS61071 Line Transient Response
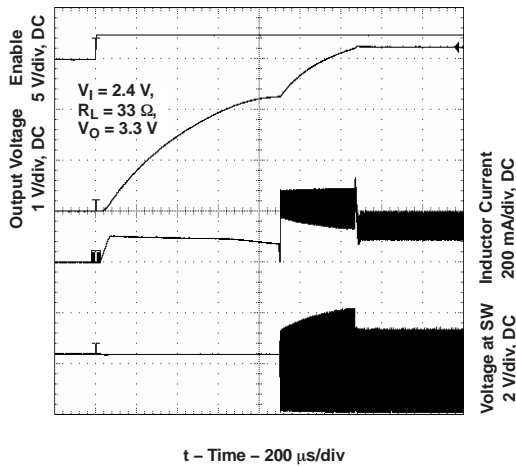
Figure 27. TPS61071 Start-Up After Enable
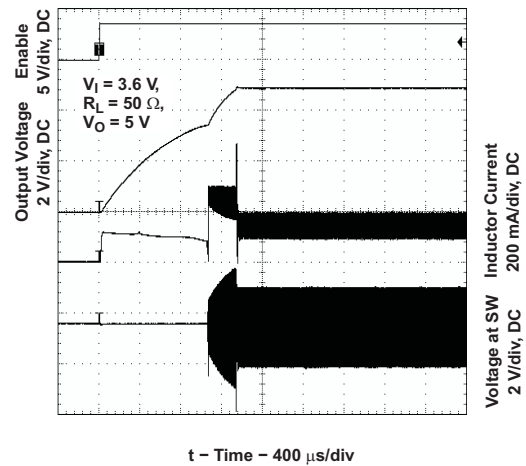
Figure 28. TPS61071 Start-Up After Enable

8.3 System Examples
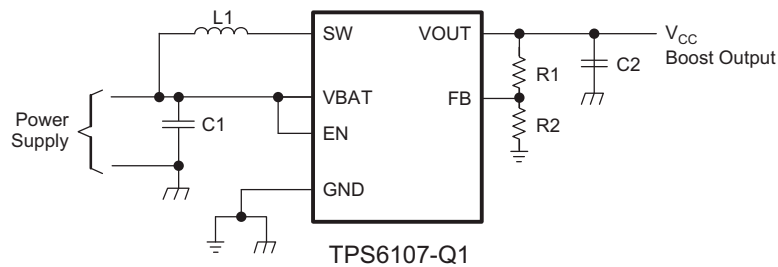
Figure 29. Power Supply Solution Having Small Total Solution Size

List of Components:
    U1 = TPS61070DDC
    L1 = 4.7 µH Taiyo Yuden CB2016B4R7M
    c1 = 1 × 4.7 µF, 0603, X7R/X5R Ceramic
    C2 = 2 × 4.7 µF, 0603, X7R/X5R Ceramic
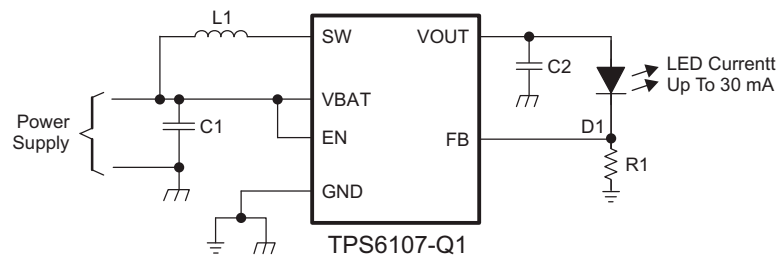
Figure 30. Power Supply Solution for Powering White LEDs in Lighting Applications

List of Components:
    U1 = TPS61070DDC
    L1 = 4.7 µH Taiyo Yuden CB2016B4R7M
    c1 = 1 × 4.7 µF, 0603, X7R/X5R Ceramic
    C2 = 2 × 4.7 µF, 0603, X7R/X5R Ceramic

Product Folder Links: *TPS61071-Q1*

System Examples (continued)
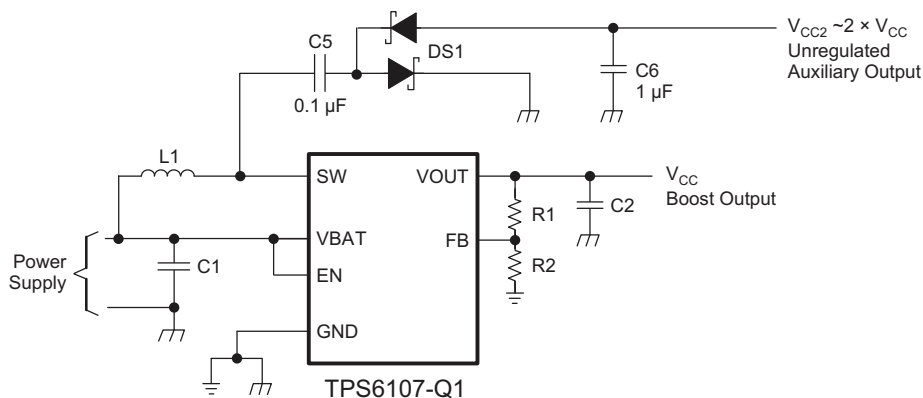
Figure 31. Power Supply Solution With Auxiliary Positive Output Voltage

List of Components:
   U1 = TPS61070DDC
   L1 = 4.7 µH Wurth Elektronik 744031004
   c1 = 2 × 4.7 µF, 0603, X7R/X5R Ceramic
   C2 = 2 × 4.7 µF, 0603, X7R/X5R Ceramic
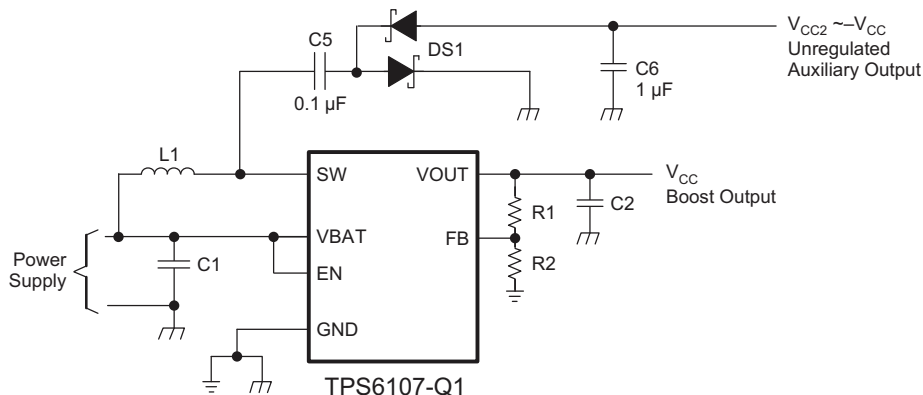
Figure 32. Power Supply Solution With Auxiliary Negative Output Voltage

List of Components:
   U1 = TPS61070DDC
   L1 = 4.7 µH Wurth Elektronik 744031004
   c1 = 2 × 4.7 µF, 0603, X7R/X5R Ceramic
   C2 = 2 × 4.7 µF, 0603, X7R/X5R Ceramic

9 Power Supply Recommendations

The TPS61071-Q1 is designed to operate from an input voltage-supply range between 0.9 V and 5.5 V. The power supply can be a DC-supply rail or one-cell, two-cell, or three-cell alkaline, NiCd or NiMH, or one-cell Li-Ion or Li-Polymer battery. The input supply should be well regulated with the rating of TPS61071-Q1. If the input supply is located more than a few inches from the device, additional bulk capacitance may be required in addition to the ceramic bypass capacitors. An electrolytic or tantalum capacitor with a value of 47 µF is a typical choice.

10 Layout

10.1 Layout Guidelines

As for all switching power supplies, the layout is an important step in the design, especially at high-peak currents and high switching frequencies. If the layout is not carefully done, the regulator could show stability problems as well as EMI problems. Therefore, use wide and short traces for the main current path and for the power ground tracks. The input capacitor, output capacitor, and the inductor should be placed as close as possible to the device. Use a common ground node for power ground and a different one for control ground to minimize the effects of ground noise. Connect these ground nodes at any place close to the ground pin of the device.

The feedback divider should be placed as close as possible to the ground pin of the device. To lay out the control ground, it is recommended to use short traces as well, separated from the power ground traces. This avoids ground shift problems, which can occur due to superimposition of power ground current and control ground current.

10.2 Layout Example
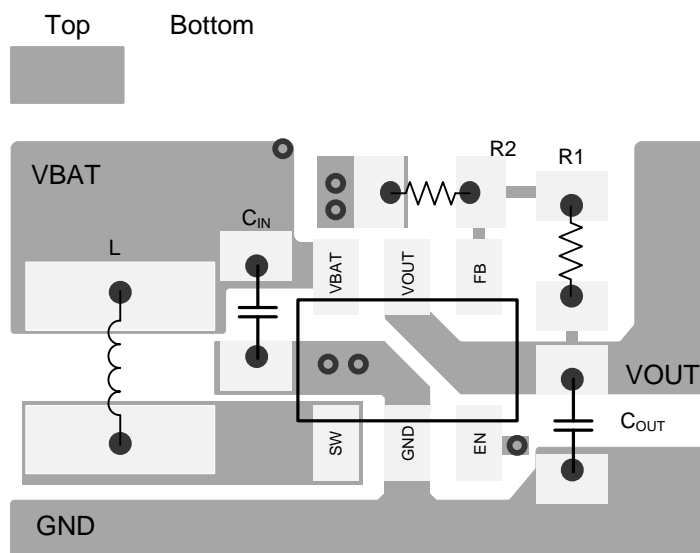
Figure 33. PCB Layout

10.3 Thermal Considerations

Implementation of integrated circuits in low-profile and fine-pitch surface-mount packages typically requires special attention to power dissipation. Many system-dependent issues such as thermal coupling, airflow, added heat sinks and convection surfaces, and the presence of other heat-generating components affect the power-dissipation limits of a given component.

There are three basic approaches for enhancing thermal performance.
- Improving the power dissipation capability of the PCB design
- Improving the thermal coupling of the component to the PCB
- Introducing airflow in the system

The maximum recommended junction temperature (T_J) of the TPS61071-Q1 device is 125°C. The thermal resistance of the 6-pin thin SOT package (DDC) is $R_{\theta JA}$ = 130°C/W. Specified regulator operation is assured to a maximum ambient temperature T_A of 85°C. Therefore, the maximum power dissipation is about 308 mW. More power can be dissipated if the maximum ambient temperature of the application is lower.

$$P_{D(MAX)} = \frac{T_{J(MAX)} - T_A}{R_{\theta JA}} = \frac{125°C - 85°C}{139.1°C / W} = 288 \text{ mW}$$

(8)

11 Device and Documentation Support

11.1 Device Support

11.1.1 Third-Party Products Disclaimer

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11.2 Community Resources

The following links connect to TI community resources. Linked contents are provided "AS IS" by the respective contributors. They do not constitute TI specifications and do not necessarily reflect TI's views; see TI's Terms of Use.

TI E2E™ Online Community *TI's Engineer-to-Engineer (E2E) Community.* Created to foster collaboration among engineers. At e2e.ti.com, you can ask questions, share knowledge, explore ideas and help solve problems with fellow engineers.

Design Support *TI's Design Support* Quickly find helpful E2E forums along with design support tools and contact information for technical support.

11.3 Trademarks

E2E is a trademark of Texas Instruments.
All other trademarks are the property of their respective owners.

11.4 Electrostatic Discharge Caution

These devices have limited built-in ESD protection. The leads should be shorted together or the device placed in conductive foam during storage or handling to prevent electrostatic damage to the MOS gates.

11.5 Glossary

SLYZ022 — *TI Glossary*.

This glossary lists and explains terms, acronyms, and definitions.

12 Mechanical, Packaging, and Orderable Information

The following pages include mechanical, packaging, and orderable information. This information is the most current data available for the designated devices. This data is subject to change without notice and revision of this document. For browser-based versions of this data sheet, refer to the left-hand navigation.

PACKAGING INFORMATION

Orderable Device	Status (1)	Package Type	Package Drawing	Pins	Package Qty	Eco Plan (2)	Lead finish/ Ball material (6)	MSL Peak Temp (3)	Op Temp (°C)	Device Marking (4/5)	Samples
TPS61071TDDCRQ1	ACTIVE	SOT-23-THIN	DDC	6	3000	RoHS & Green	NIPDAU	Level-1-260C-UNLIM	-40 to 105	DAY	Samples

(1) The marketing status values are defined as follows:
ACTIVE: Product device recommended for new designs.
LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.
NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.
PREVIEW: Device has been announced but is not in production. Samples may or may not be available.
OBSOLETE: TI has discontinued the production of the device.

(2) RoHS: TI defines "RoHS" to mean semiconductor products that are compliant with the current EU RoHS requirements for all 10 RoHS substances, including the requirement that RoHS substance do not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, "RoHS" products are suitable for use in specified lead-free processes. TI may reference these types of products as "Pb-Free".
RoHS Exempt: TI defines "RoHS Exempt" to mean products that contain lead but are compliant with EU RoHS pursuant to a specific EU RoHS exemption.
Green: TI defines "Green" to mean the content of Chlorine (Cl) and Bromine (Br) based flame retardants meet JS709B low halogen requirements of <=1000ppm threshold. Antimony trioxide based flame retardants must also meet the <=1000ppm threshold requirement.

(3) MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

(4) There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.

(5) Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.

(6) Lead finish/Ball material - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

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In no event shall TI's liability arising out of such information exceed the total purchase price of the TI part(s) at issue in this document sold by TI to Customer on an annual basis.

OTHER QUALIFIED VERSIONS OF TPS61071-Q1 :

● Catalog: TPS61071

NOTE: Qualified Version Definitions:

   ● Catalog - TI's standard catalog product

PACKAGE MATERIALS INFORMATION

TAPE AND REEL INFORMATION

REEL DIMENSIONS

TAPE DIMENSIONS

A0	Dimension designed to accommodate the component width
B0	Dimension designed to accommodate the component length
K0	Dimension designed to accommodate the component thickness
W	Overall width of the carrier tape
P1	Pitch between successive cavity centers

QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE

*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
TPS61071TDDCRQ1	SOT-23-THIN	DDC	6	3000	179.0	8.4	3.2	3.2	1.4	4.0	8.0	Q3

![Texas Instruments logo] **PACKAGE MATERIALS INFORMATION**

TAPE AND REEL BOX DIMENSIONS

*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
TPS61071TDDCRQ1	SOT-23-THIN	DDC	6	3000	200.0	183.0	25.0

4214841/C   04/2022
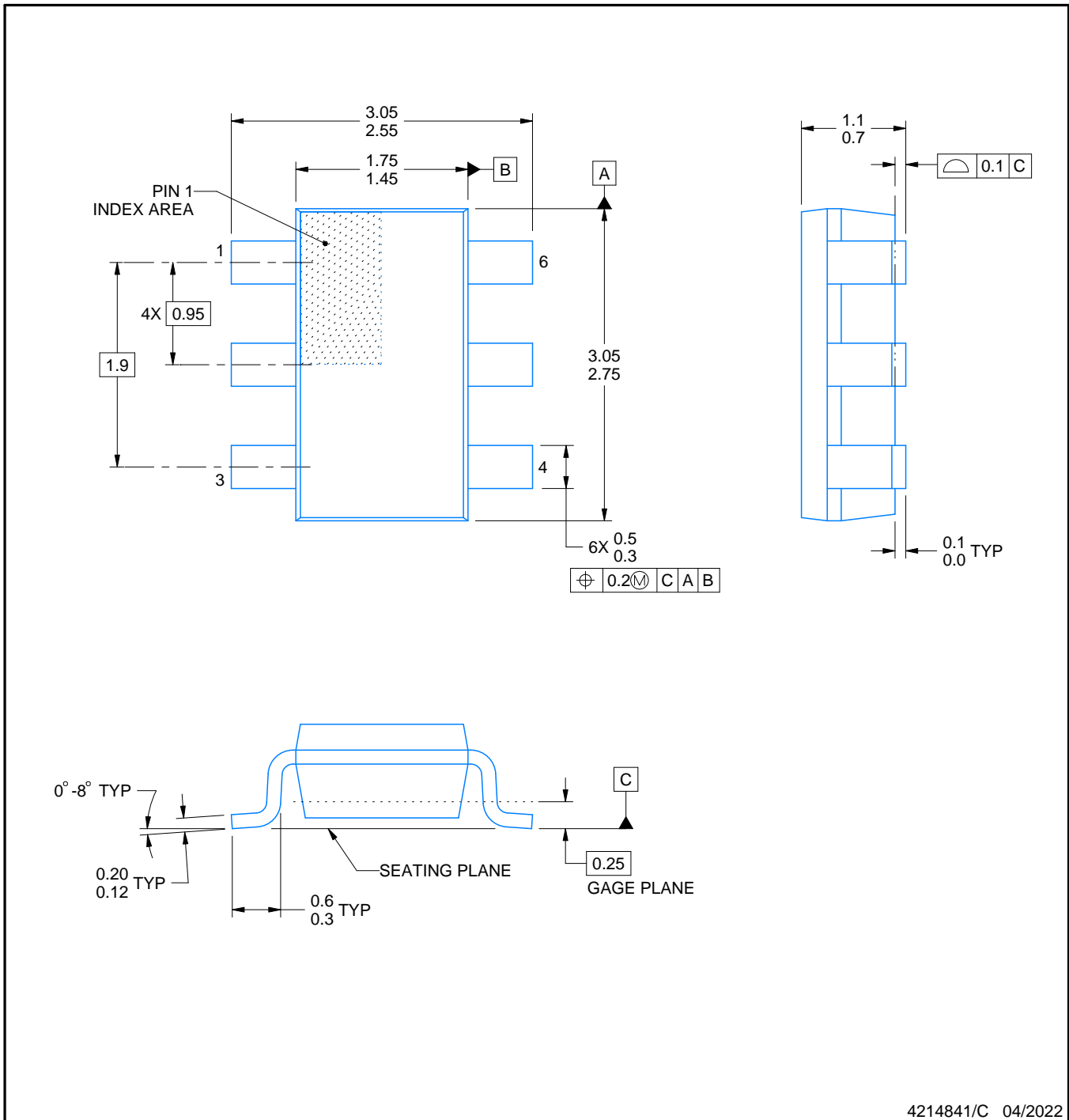
NOTES:

1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
2. This drawing is subject to change without notice.
3. Reference JEDEC MO-193.

SYMM

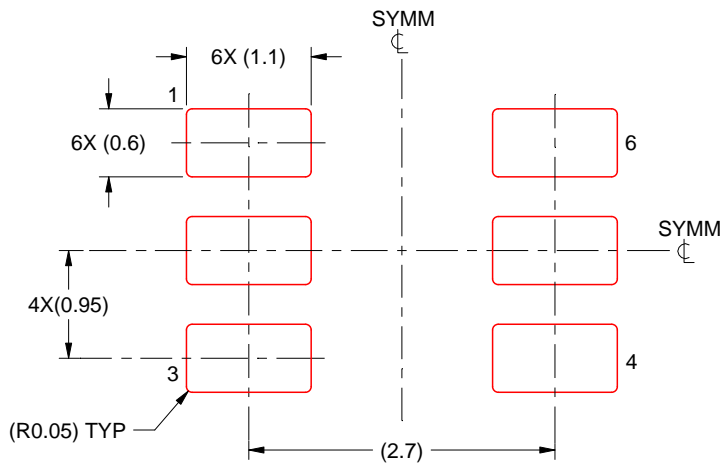6X (1.1)

1

6X (0.6)

6

SYMM

4X (0.95)

3

4

(R0.05) TYP

(2.7)

LAND PATTERN EXAMPLE
EXPLOSED METAL SHOWN
SCALE:15X

SOLDER MASK
OPENING

METAL

EXPOSED METAL

0.07 MAX
ARROUND

NON SOLDER MASK
DEFINED

METAL UNDER
SOLDER MASK

SOLDER MASK
OPENING

EXPOSED METAL

0.07 MIN
ARROUND

SOLDER MASK
DEFINED

SOLDERMASK DETAILS

4214841/C 04/2022

NOTES: (continued)

4. Publication IPC-7351 may have alternate designs.
5. Solder mask tolerances between and around signal pads can vary based on board fabrication site.

SOLDER PASTE EXAMPLE
BASED ON 0.125 THICK STENCIL
SCALE:15X

4214841/C 04/2022

NOTES: (continued)

6. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate
   design recommendations.
7. Board assembly site may have different recommendations for stencil design.

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